Development of Real-Time Electromyography Controlled 3D Printed Robot Hand Prototype

Preliminary Communication

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Abstract – Developing an anthropomorphic robotic hand (ARH) has become a relevant research field due to the need to help the amputees live their life as normal people. However, the current state of research is unsatisfactory, especially in terms of structural design and the robot control method. This paper, which proposes a 3D printed ARH structure that follows the average size of an adult human hand, consists of five fingers with a tendon-driven actuator mechanism embedded in each finger structure. Besides that, the movement capability of the developed 3D printed robot hand validated by using motion capture analysis to ensure the similarity to the expected motion range in structural design is achieved. Its system functionality test was conducted in three stages: (1) muscular activity detection, (2) object detection for individual finger movement control, and (3) integration of both stages in one algorithm. Finally, an ARH was developed, which resembles human hand features, as well as a reliable system that can perform opened hand palm and some grasping postures for daily use.

Keywords – anthropomorphic robotic hand (ARH), electromyography (EMG), reliable system, robot hand.

1. INTRODUCTION

In 2012, about 350,000 out of the total of 29.5 million Malaysian population were registered as disabled, and more than 100,000 people were categorized as upper limb amputees and paralyzed with physical disabilities [1]. The fact shows how vital research is related to the development of a robot hand device as a way to help these people perform their daily activities as a normal human does. The anthropomorphic robot hand is one of the robot hand device classes which resembles the human hand. Thus, it emphasizes the reliability and aesthetic value of the device [2]. The device normally is less complex and able to perform a simple task such as opened hand palm and basic grasping postures. A hand prosthesis device should be capable of operating full day that may include the energy harvesting mechanism [3-8] to limit the number of battery charging cycles [9].

In recent decades, robot hand control has undergone evolution, and the conventional joystick controller is not the only interface that can be used as a robot control interface. There are many alternatives to the robot control interface available such as an electromyography (EMG) sensor and many more. An EMG sensor is used to provide muscular activity information as inputs for the system. It becomes the most frequently used robot control interface due to its transparent characteristic, which allows the user to control the robot as their body part [10, 11]. Besides, it is a non-invasive and easy-to-use sensor. In an effort to support the growth of the robot hand research field, 3D printed technology has become the best fabrication method option for this application, as recommended in Industrial Revolution 4.0. It triggers a massive revolution in robot hand production to produce printable prosthetic hand design which is customizable to the wearer and can be printed easily by anyone and anywhere virtually [12].

Recently, some of the researchers have produced robots that have incomplete fingers that do not resemble the actual anatomy of the human hand. They applied the cable-driven actuator mechanism into structural design [13-18]. We found that the mechanism negatively affects motion accuracy of the joint due to the elastic characteristic of the material itself [19, 20]. Besides, several kinds of research came out with five fingers and the tendon-driven actuator mechanism, but finger movement does not actuate individually [21], and it is bigger than the average size of an adult human hand [22]. We also found that robot structure made of metal [23] is heavy and difficult to be fabricated compared to a 3D printed product in terms of cutting and shaping the product. Currently, 3D printed technology has gained attention of researchers working on a prosthesis hand [14, 16, 18, 24], and it became the fabrication method most frequently used for this purpose.

This paper describes robot hand structural design that follows the average size of an adult human hand and fabricates it by means of 3D printing technology as a recommended fabrication method in the previous study. We hypothesized that the 3D printed robot structure with a tendon-driven actuator mechanism could achieve optimum similarity to the expected motion range as in structural design. For robot control, integration of both an EMG sensor and infra-red sensors into the system allows five fingers to move individually.

2. METHODOLOGY

Fig. 1 shows an overview of the project; this research started with two streams simultaneously categorized as structure and system development. In terms of structure development, it consists of a review of current research on structural design of the robot hand and a list of features applied to structural design as improvement. Robot structural design was visualized in a three-dimensional view. Next, finalized structure design was fabricated by using 3D printing technology. In terms of system development, circuit design of the system was constructed, and the electronic hardware components were assembled. Then, the electronic components were combined with the 3D printed robot structure to complete a prototype. The movement capability of the printed product was examined through motion analysis by using motion capture equipment. Finally, the prototype will be tested for its functionality and reliability to perform several hand postures.

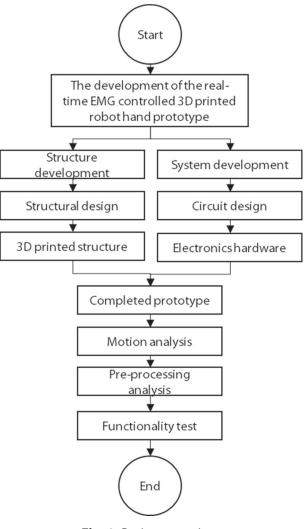


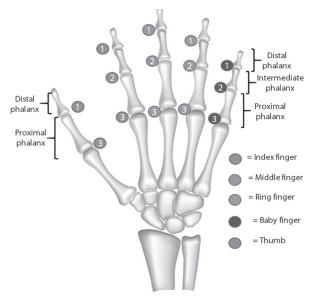
Fig. 1. Project overview.

2.1. STRUCTURAL DESIGN

This section shows the features of robot hand structural design to improve robot hand structural design of the previous study. The design is illustrated in threedimensional (3D) drawing using computer-aided software called Inventor Professional 2018 (Autodesk). The features applied in the design are listed below:

Five fingers with individual movement. Each human hand consists of five fingers that move independently of each other. The fingers are known as the thumb, index, middle, ring and baby fingers. Each finger has three bones known as distal phalanx (DP), intermediate phalanx (IP) and proximal phalanx (PP), with the exception of the thumb that has only DP and PP. In the middle of two bones there are joints known as distal interphalangeal (DIP), proximal interphalangeal (PIP)

and metacarpophalangeal (MCP). These joint locations are shown in Fig. 2. The number degree of freedom (DOF) of the robot hand is the same as the number of joints involved in structural design, and it is about 14 DOFs. Each finger is allocated one actuator.



- Fig. 2. Human skeletal hand structure: 1 = Distal interphalangeal, 2= Proximal interphalangeal, 3= Metacarpophalangeal.
- The planar rigid body motion limits on the sagittal plane only, as shown in Fig. 3.

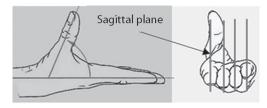
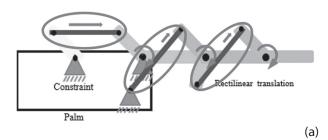


Fig. 3. Sagittal plane of the planar rigid body.

 Tendon-driven actuator mechanism, as shown in Fig. 4. This mechanism uses a solid connector that connects the actuator and robot structure to improve the motion range accuracy of the current robot hand structural design with a cabledriven actuator mechanism. The extension and flexion motion of the finger are shown in Fig. 4(a) and 4(d), respectively.



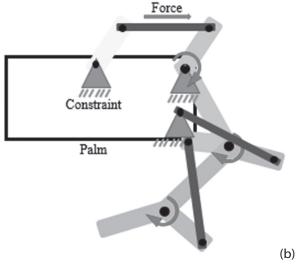


Fig. 4. Robot structure with a tendon-drive actuator: (a) extension motion, (b) flexion motion.

• The thumb tilted 45° to the left and normal to the hand palm, as shown in Fig. 5. This feature is used to improve the handgrip of the grasping posture.

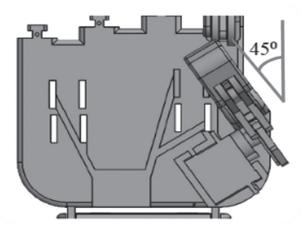


Fig. 5. The thumb of the robot hand tilted 45° to the left.

 Follow the average size of the adult human hand as an effort to make a robot that resembles an actual human hand [20]. The details of the finger bone lengths are shown in Table 1.

Table 1. The	lengths of	finger bones
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Index, Middle, Ring	Thumb	
Name of bone	Length (m)	Length (m)
DP	0.02325	0.02325
IP	0.02400	-
PP	0.03960	0.03960

• Limits the motion range of the joints by applying the mechanical stopper to design, as shown in Fig. 6. The details of the motion range of the joint are shown in Table 2.

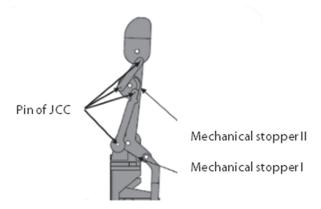


Fig. 6. Mechanical stopper of the finger structure.

Table 2. Mechanica	l stopper of the	finger structure.
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lainta		Fingers
Joints	Joints Thumb	Index, Middle, Ring, Baby
DIP	85°	90°
PIP	-	105°
МСР	90 [°]	85°

2.2. CIRCUIT DESIGN AND ELECTRONICS HARDWARE

By referring to the block diagram shown in Fig. 7 and the electronic hardware configuration of the system shown in Fig. 8, there are two detections involved in the system known as muscular activity and object detection. For muscular activity detection, it was performed by using the Myoware EMG sensor, while object detection was performed by using four units of S-LFS-4-4 ways IR sensors. These sensors act as the input interface of the processor (the Arduino Uno microcontroller). The microcontroller used to process the input signal and control the (TowerPro SG90) servo motor (five units). The movements are produced because the tendon mechanism connects the actuator to the robot structure. The signals can be monitored by connecting the microcontroller to the laptop through a universal serial bus port. The power source of the system is supplied from the power grid (240V 60Hz), and it is converted into DC power supply (5V 2A) by using a DC-DC converter.

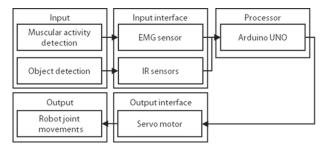


Fig. 7. A block diagram of the system.

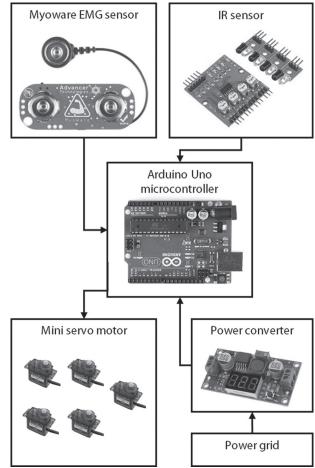


Fig. 8. Electronics hardware configuration of the system.

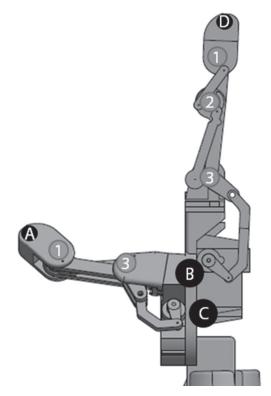


Fig. 9. Reflective marker placement setup: 1 = distal interphalangeal, 2= proximal interphalangeal, 3= metacarpophalangeal.

2.3. COMPLETED PROTOTYPE

2.3.1. Motion analysis

The motion capture experiment is the motion analysis of the moving part of the actual finger structure. This experiment is used to measure the maximum and minimum motion range of each joint, and the results were compared to the expected motion range, as mentioned in Table 2 above. The equipment used in this experiment were eight units of OptiTrack Flex 13 motion tracking cameras, a unit of Basler acA640-120gs synchronizing camera and nine units of reflective markers. Reflective markers are set up on the structure, as shown in Fig. 9. The robot structure acts as a subject placed in the middle of the workspace and all cameras face the subject, as shown in Fig. 10. The robot structure was controlled to perform opened hand palm and grasping motion postures for alternately 2 seconds, repeated three times for each sample. The samples were recorded five times using Venus 3D software with a 100Hz sampling rate.

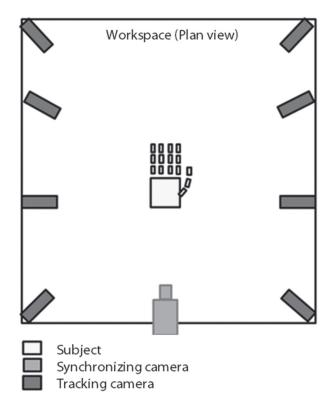


Fig. 10. Motion capture experimental setup

2.3.2. Electromyography (EMG) sensors placement and pre-processing analysis

The EMG sensor was attached to the skin, where the flexor digitorum superficial (FDS) muscle is located. The FDS is the muscle used to flex the fingers, and it is suitable for muscle flexion [25]. The EMG signal was collected by using the MyoWare EMG sensor with a sampling rate of 100Hz. Next, the pre-processing analysis of the EMG signal was done to improve the signal quality. The analysis consists of three stages such as magnitude nor-

malization, rectification, and noise filtration, as shown in Fig. 11. After that, the threshold voltage was fixed at 0.02V due to less oscillation occurring at this magnitude.



Fig. 11. Pre-processing analysis process

2.3.3. System functionality test

The functionality test was conducted in three stages: muscular activity detection only, object detection only, and integration of both muscular activity detection and object detection.

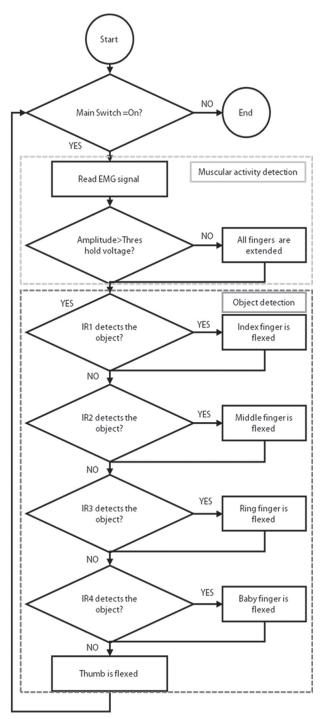
For the first stage, the EMG sensor is used to measure the signal generated from the targeted muscle. The signal is generated when the flexion and extension motion are done by the muscle. When the muscle flexes, the amplitude of the EMG signal is higher than usual. Thus, if the EMG signal amplitude generated more than the threshold voltage (THV) value, the robot hand would grasp the object. The robot was tested to detect the opened hand palm and grasping postures for five times alternately with 1s for each posture and control robot movements in real-time. This procedure was repeated for two trials to get an accurate result.

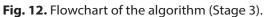
For the second stage, it is more likely to make a variation of the robot hand posture by using the object detection method. There are four infra-red (IR) sensors used, and a sensor was allocated to each finger: index, middle, ring and baby fingers. When the IR sensor detects the object, the finger structure aligned to the sensor will be flexed. The sensors were tested for two trials by placing the obstacle on the hand palm as following motion steps, as listed in Table 3. The selected motions of the robot hand posture are commonly used in human daily life activities [26].

For the third stage, both muscular activity and object detection were integrated into one algorithm, as shown in Fig. 12. The robot system will be started with muscular activity as the first condition, and then it will proceed to object detection, as mentioned in the second stage of the functionality test. This procedure was repeated for two trials.

Table 3. Motion	steps of the object	t detection test.
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	Object Detection						
Step	IR1	IR2	IR3	IR4			
1	On	Off	Off	Off			
2	On	On	Off	Off			
3	On	On	On	Off			
4	On	On	On	On			





3. RESULTS AND DISCUSSION

3.1. 3D PRINTED ROBOT HAND STRUCTURE AND ITS ELECTRONIC HARDWARE

The finger structure consists of some of the 3D printed parts as body structure, and some of the steel parts such bolts and nuts as the joint connector, as shown in Fig. 13. Fig. 14 shows that the complete prototype of the robot hand is the integration of the structure and electronic hardware.

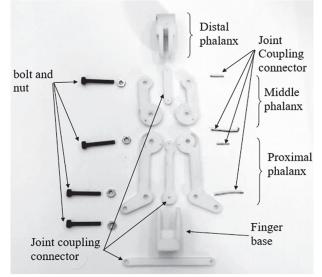


Fig. 13. Components of the finger structure - disassembled

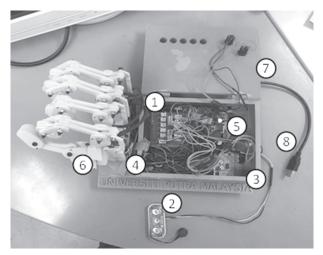


Fig. 14. Complete prototype (1) Arduino Uno board, (2) Myoware EMG sensor, (3) IR sensor, (4 & 5) DC-DC converter, (6) robot hand structure, (7) buttons, and (8) power supply adaptor.

3.2. MOTION ANALYSIS

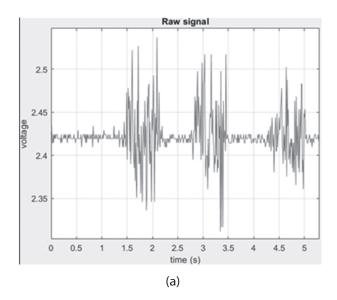
There were limitations in the experiment. Reflective markers could not be placed on all fingers, except the thumb and index finger due to insufficient space. Thus, reflective markers were placed on the index finger and the thumb only, and the index finger was assumed to be similar to the middle, ring, and baby finger due to identical structural design. Besides, the experiment was done to ensure the movement capability of the joint of the 3D printed structure reaching the optimum similarity to the expected motion range of structural design of the structure. By referring to Table 4, we can see that motion similarity between the 3D printed robot hand structure and structural design ranges between 72.62 and 98.43%.

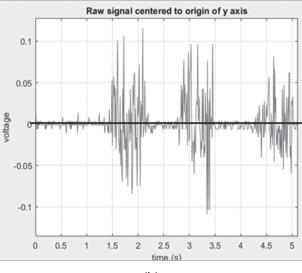
structure design and actual finger									
	Thumb								
Joint	Min.	Max.	Measured ROM	Expected ROM	Similarity				
DIP	76.1969°	159.8606°	83.6637°	85°	98.43%				
MCP	95.2821°	172.8265°	77.5444°	90°	86.16%				
			Index						
	Min.	Max.	Measured ROM	Expected ROM	Similarity				
DIP	90.6170°	165.0229°	74.4059°	90°	82.67%				
PIP	101.5059°	177.7636°	76.2577°	110°	72.62%				

Table 4. Range of motion (ROM) of the joint forstructure design and actual finger

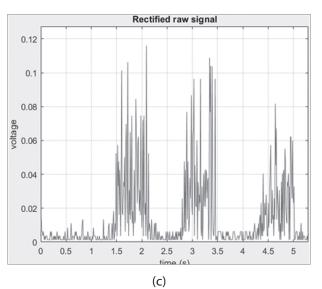
3.3. ELECTROMYOGRAPHY (EMG) SIGNAL PRE-PROCESSING

Fig. 15 shows the changes that occurred toward the EMG signal for every stage of the pre-processing analysis. The raw signal generated from the sensor is highly oscillating due to the presence of the noise signal, as shown in Fig. 15(a). After that, the signal magnitude is normalized, when the mid-value of the signal is moved to zero on the y-axis, as shown in Fig. 15(b). This being the case, the signal has two sides of magnitude, i.e., a positive and a negative value. Next, the signal is rectified, as shown in Fig. 15(c), so a negative magnitude of the signal is moved to the positive side of the magnitude. Then the rectified signal (red line) is smoothed as a blue line shown in Fig. 15(d) by applying the Butterworth low pass signal with 0.03Hz of the cut-off frequency obtained from the magnitude spectrum graph, as shown in Fig. 16.









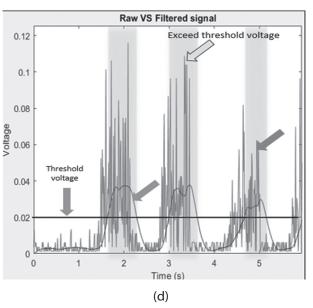
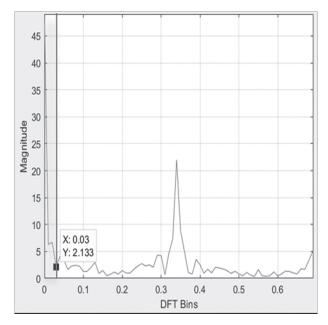


Fig. 15. Pre-processing analysis of the EMG sensor output (a) Raw signal, (b) Magnitude normalization, (c) Rectification, (d) Noise filtration.



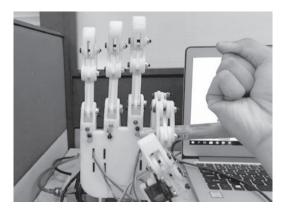


3.4. FUNCTIONALITY TEST

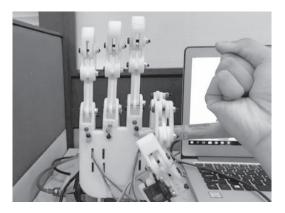
System functionality was evaluated through some trials carrying out some tasks as mentioned in Section 2.3.3 and the result shown in Table 5. In the first stage, robot control based on the EMG sensor to perform grasping and hand palm opening was performed for five times with two trials, while the robot also succeeded to perform four different grasping postures based on object detection of the IR sensor in the second stage. In the third stage, the integration of two previous stages into one algorithm worked without any failure, as shown in Fig. 17. As a conclusion, robot control of the robot hand prototype is reliable.

Stag	Trial							Suc.				
Stag	Conditi			1					2			Rate
1 st	Amp>THV	1	2	3	4	5	1	2	3	4	5	10004
1	Status	~	\checkmark	√	~	~	~	~	~	~	~	100%
2 ND	Step	1	2	3	4		1	2	3	4		1000/
Z	Status	~	\checkmark	\checkmark	\checkmark		~	~	\checkmark	\checkmark		100%
	Amp>THV	1	2	3	4		1	2	3	4		
BD	Status	~	\checkmark	\checkmark	~		~	~	~	\checkmark		1000/
3 RD	Step	1	2	3	4		1	2	3	4		100%
	Status	\checkmark	\checkmark	\checkmark	\checkmark		~	\checkmark	√	v		

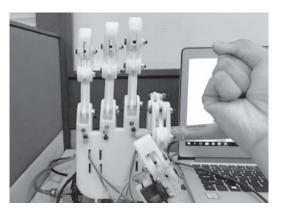
Table 5. System functionality evaluation result	Table 5. S	ctionality evaluation re	sult.
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(a)



(b)



(c)

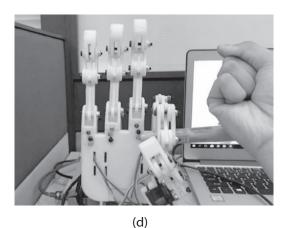


Fig. 17. Robot hand motion: (a) Step 1, (b) Step 2, (c) Step 3, and (d) Step 4.

4. CONCLUSION

In conclusion, a real-time EMG controlled 3D printed robot hand prototype with improved features of structural design was developed, and its reliability was proven through the conducted functionality test.

For further study, an advanced controller using artificial intelligence could be applied to the system.

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